

**DATUM INFORMATION**  
NANNAQUAKET, RI 8450954

**SURVEY NOTE:**  
CLASS 1 BOUNDARY SURVEY  
PERFORMED BY:  
JOHN BARKER, PLS  
168 HIGH STREET  
BRISTOL, RI 02809  
401.254.0824

NOTE:  
ALL ELEVATIONS ARE IN REFERENCE TO  
MLW DATUM (SEE TIDAL CHART ABOVE)

**DOCK AREA:**  
4'x39' FIXED DOCK = 156 SF  
4'x30' SLOPED DOCK = 120 SF  
6'x8' FIXED DOCK = 32 SF  
3'x24' GANGWAY = 72 SF  
4'x20' TERMINAL = 80 SF  
TOTAL DOCK AREA = 460 SF  
TOTAL AREA PAST MHW = 335 SF

**OWNER/APPLICANT**  
MARC DEMELLO

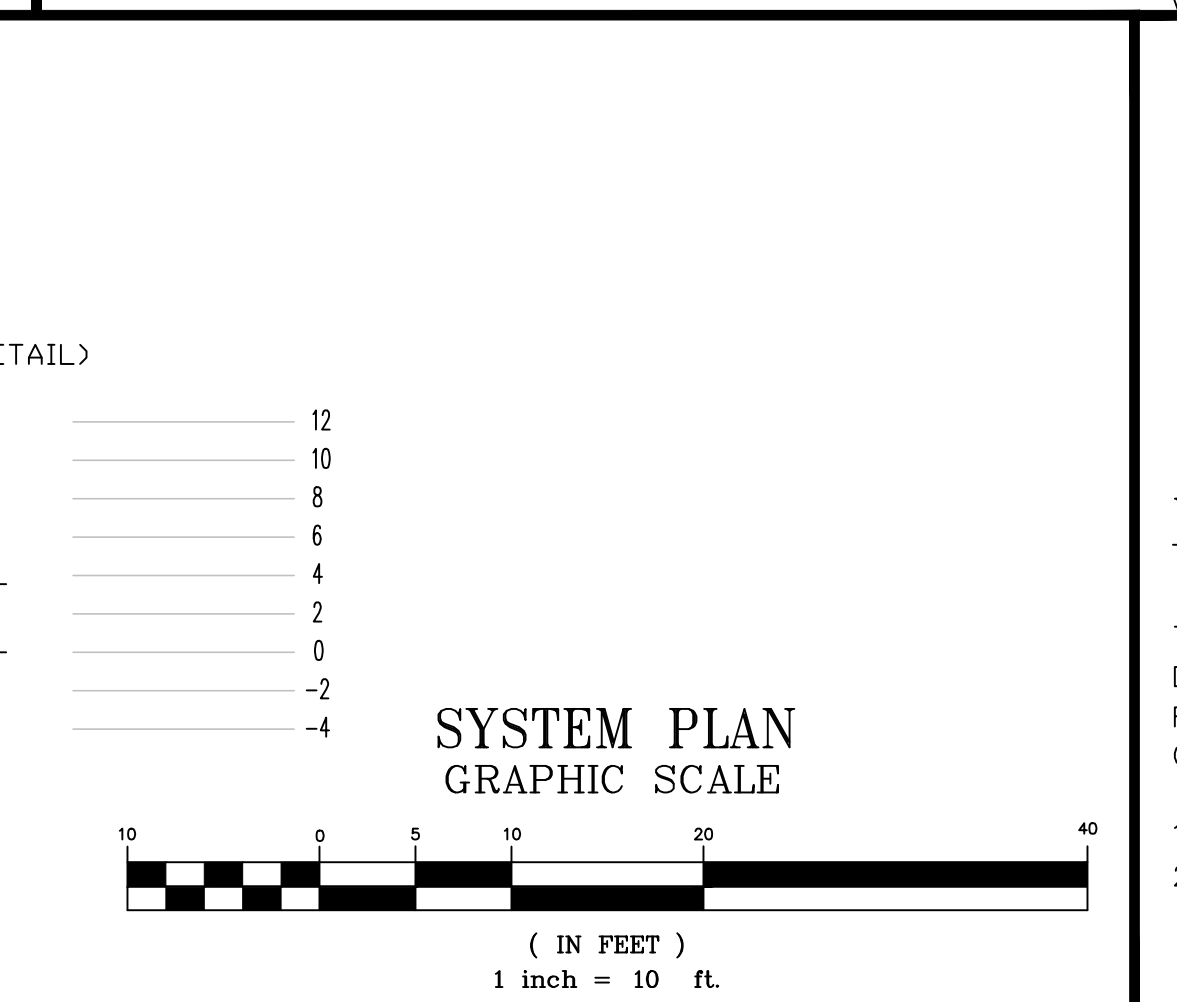
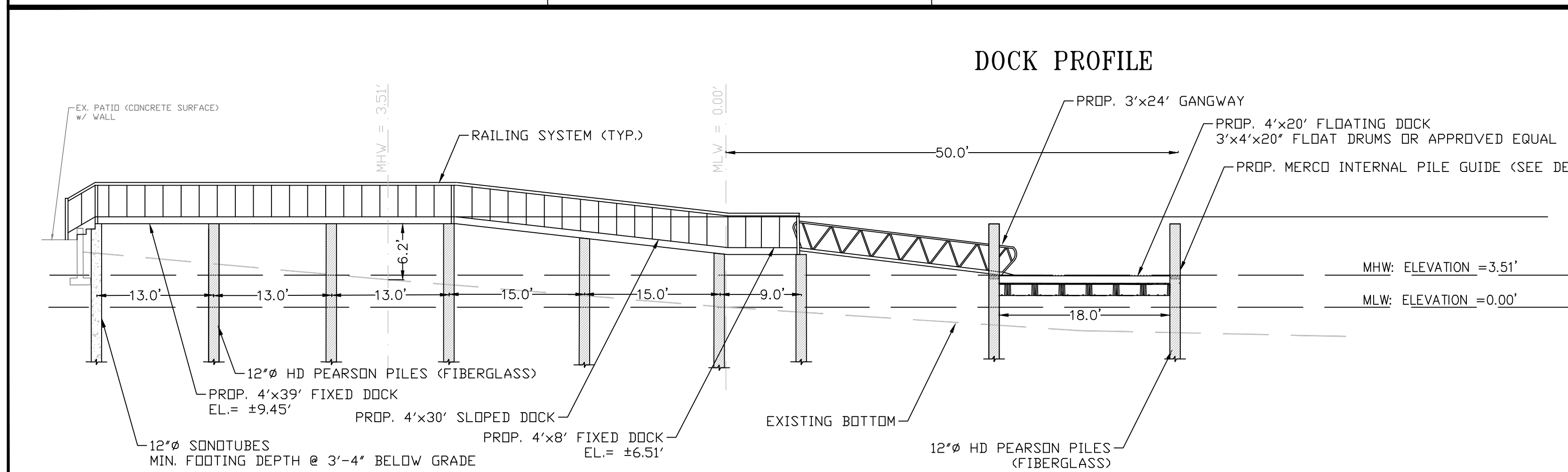
No.	Revision/Issue	Date
1	REMOVAL OF BOAT LIFT	8/23

**PRINCIPE COMPANY, INC.**  
ENGINEERING DIVISION  
ESTABLISHED IN 1961

PO BOX 298  
TIVERTON, RI 02878  
PHONE: 401.265.1090  
EMAIL: PRINCIPEENGINEERING@GMAIL.COM  
WWW.PRINCIPEBUILDERSRI.COM

**NEW DOCK PLANS**  
for  
**AP 25 LOT 45**  
**395 PARK AVENUE**  
in  
PORTSMOUTH, RHODE ISLAND

Date	Sheet
04/28/2023	1 OF 3



**ZONING (R10):**

REGULATION:  
10,000 SF  
100 FT  
20 FT  
20 FT  
10 FT  
20%  
35 FT

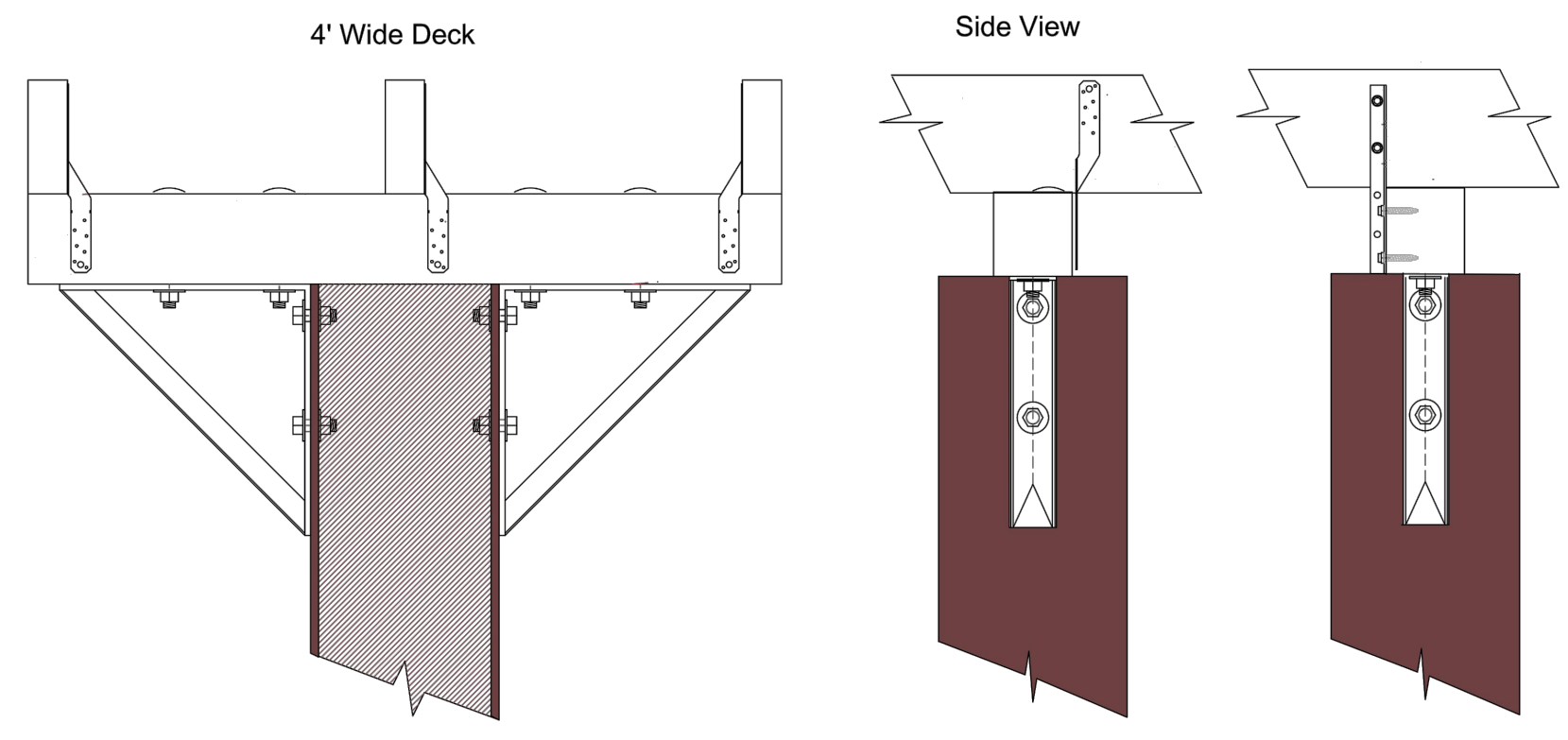
MIN. LOT AREA:  
MIN. FRONT YARD:  
MIN. REAR YARD:  
MIN. SIDE YARD:  
MAX. LOT COVERAGE:  
MAX. BUILDING HEIGHT:

**VARIANCE NOTE:**  
THE FOLLOWING ARE A LIST OF ITEMS THAT DO NOT FULLY MEET CRMC'S RULES AND REGULATIONS DUE TO EXISTING SITE CONSTRAINTS AND ARE REQUESTING RELIEF:

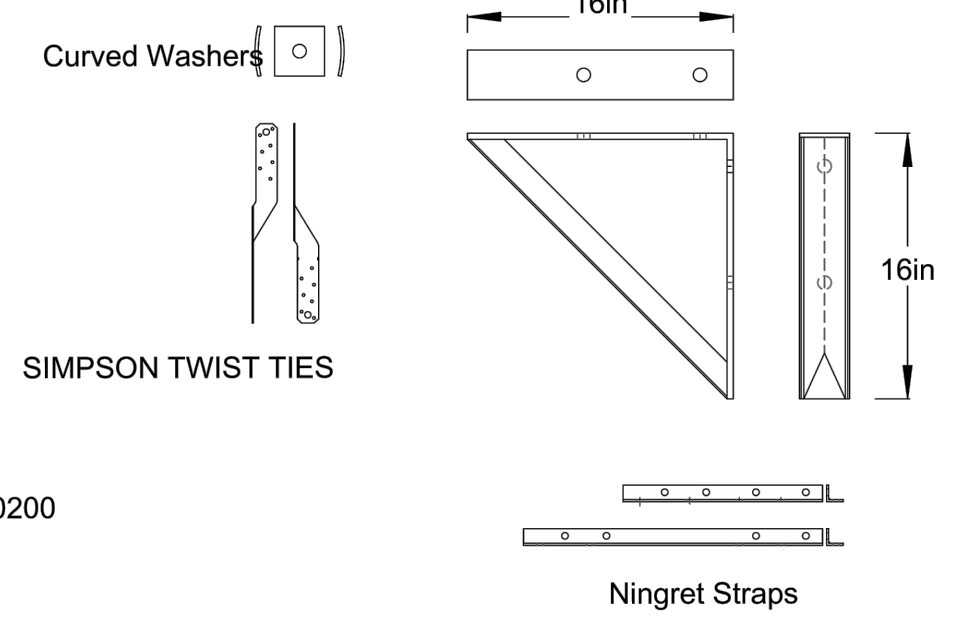
1.) PROPERTY LINE (EXTENSION) SETBACK - 25' MIN. REQUIRED  
-13.5' PROVIDED

Thomas J. Principe, III  
REGISTERED PROFESSIONAL ENGINEER





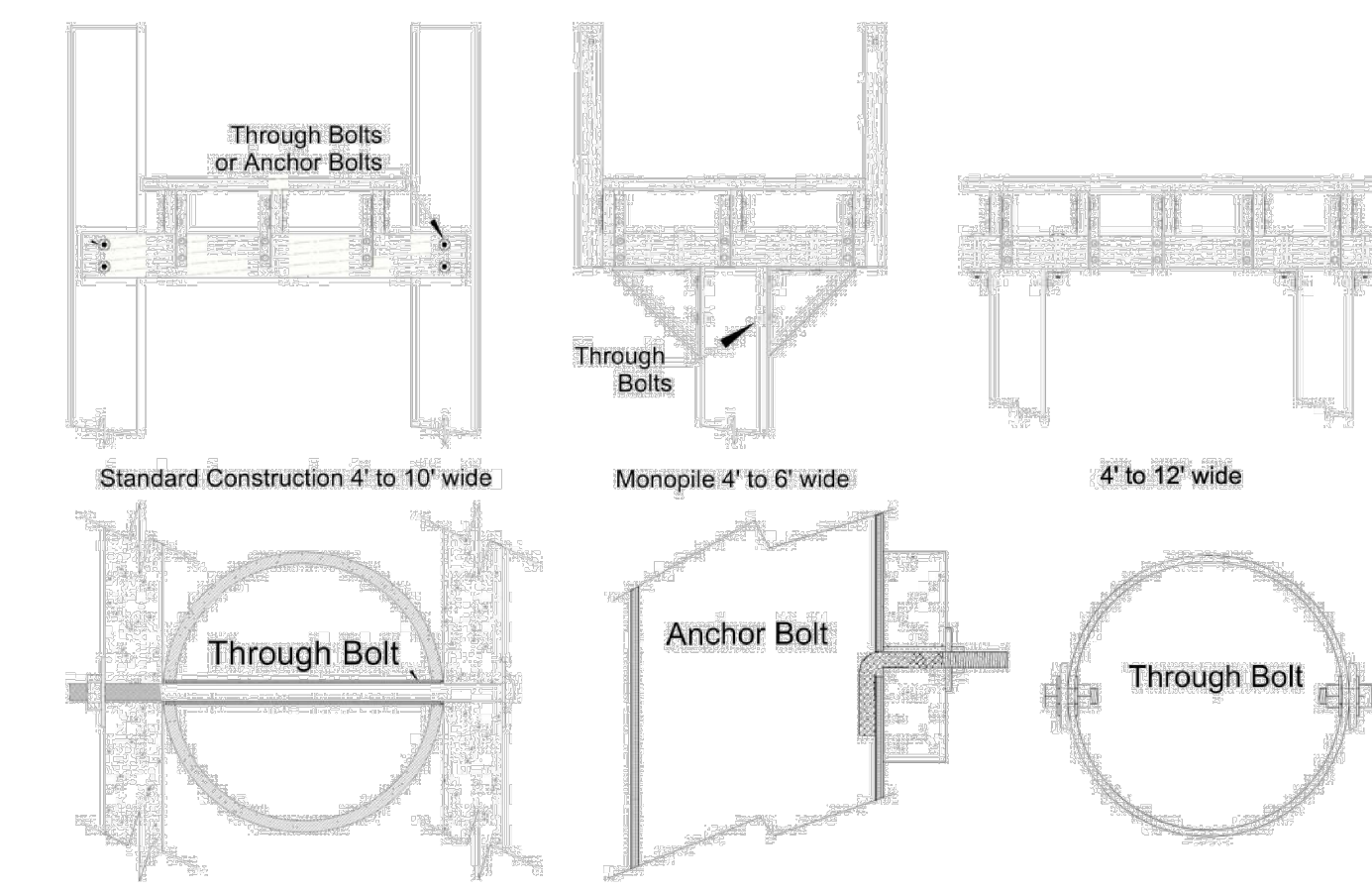
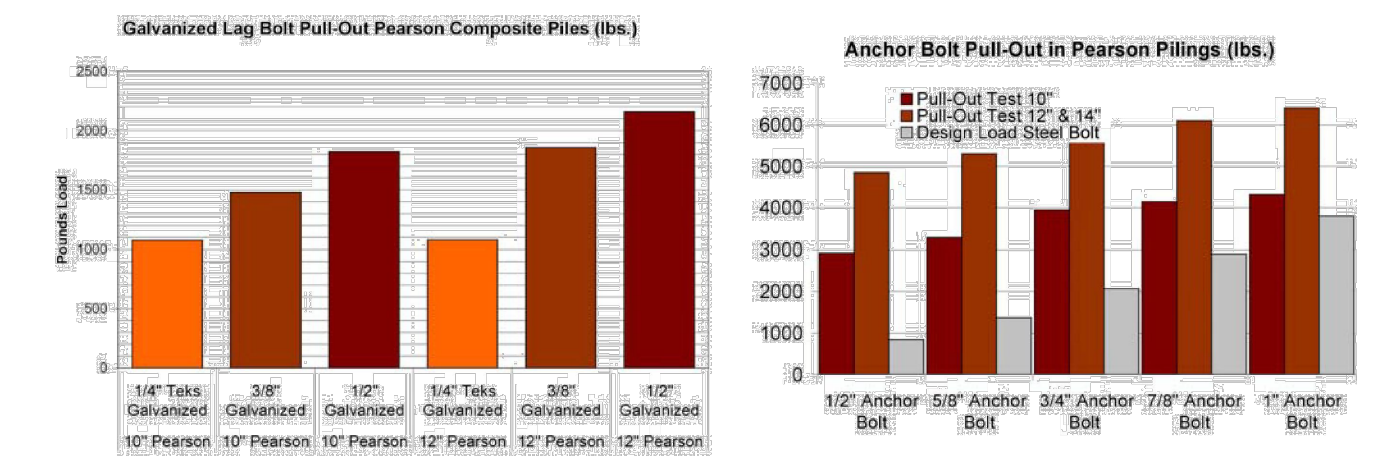
- Monopile Requirements:**
- 2 Monopile Brackets
  - 4 x 6 P.T. Beam (Pile Cap) for 4' wide deck
  - 4 - 3/4 x 2 Galvanized bolts
  - 8 - 3/4" Galvanized Standard Washers
  - 4 - 3/4" Galvanized Curved Washers
  - 4 - 3/4 x 8 Galvanized Timber Bolts (6" Timber)
  - Simpson MTS12 Twist Strap 16 ga.
  - 10d galvanized nails
  - (or Ningret Straps & Bolts) Ningret Marine - (401) 364-0200



**Attachment and Assembly Data**

Due to the three dimensional fiber architecture of Pearson Pilings fiberglass reinforcements, through-bolts and anchor bolts are all used for various installations and applications. Even lag bolts can be used for non-structural fastening. The holding and pull-out strength of bolted connections to the composite pile typically exceed the operating load recommendations for galvanized bolts as shown below. Structural cross members, beams, boat lifts and ramp hardware should be attached using either anchor bolts or through bolts.

Lag bolts may be used for non-structural connections and fitting of cleats, line holders, hand rails, fenders, ladders, benches and lighting fixtures. 1/2" Washer Head Tek screws should be used for attaching pile caps - most self tapping screws will work, but avoid those with flanges on the drill section.



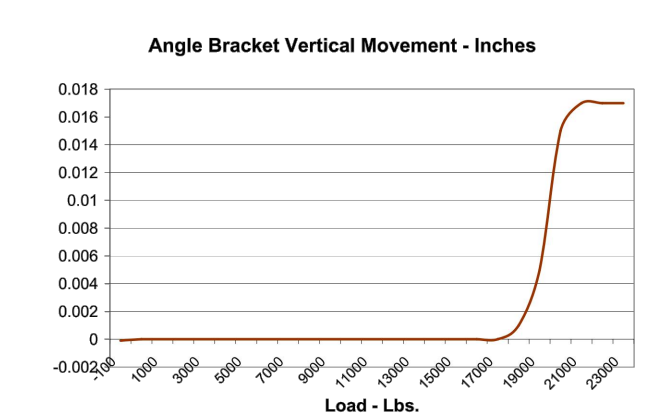
© 2007 Pearson Pilings LLC



**Pearson Pilings Testing Angle Bracket / 3/4" Bolts**

In order to determine recommended loading for the use of galvanized brackets with a single 3/4" bolt, an axial load test was performed. To simplify the fixture, the 4" square brackets were attached to the end of a 10" diameter pile so that the flats were above the pile top by .250".

The elongation in the pile wall did not propagate from 18,000 lbs. to 23,000 lbs. at which point the 3/4" bolts started to deform. The test was discontinued at this point.



Assembled Brackets - 10" Pile

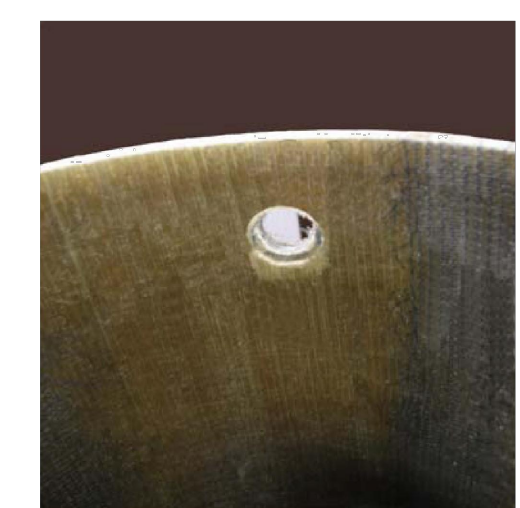


18,000 lb load distributed over 2 brackets

The load was applied in increments of 1,000 lbs. - there was a compressive deformation in the composite pile wall at 18,000 lbs. total load (9,000 lbs. per bracket).



Bolt Hole Elongation - exterior



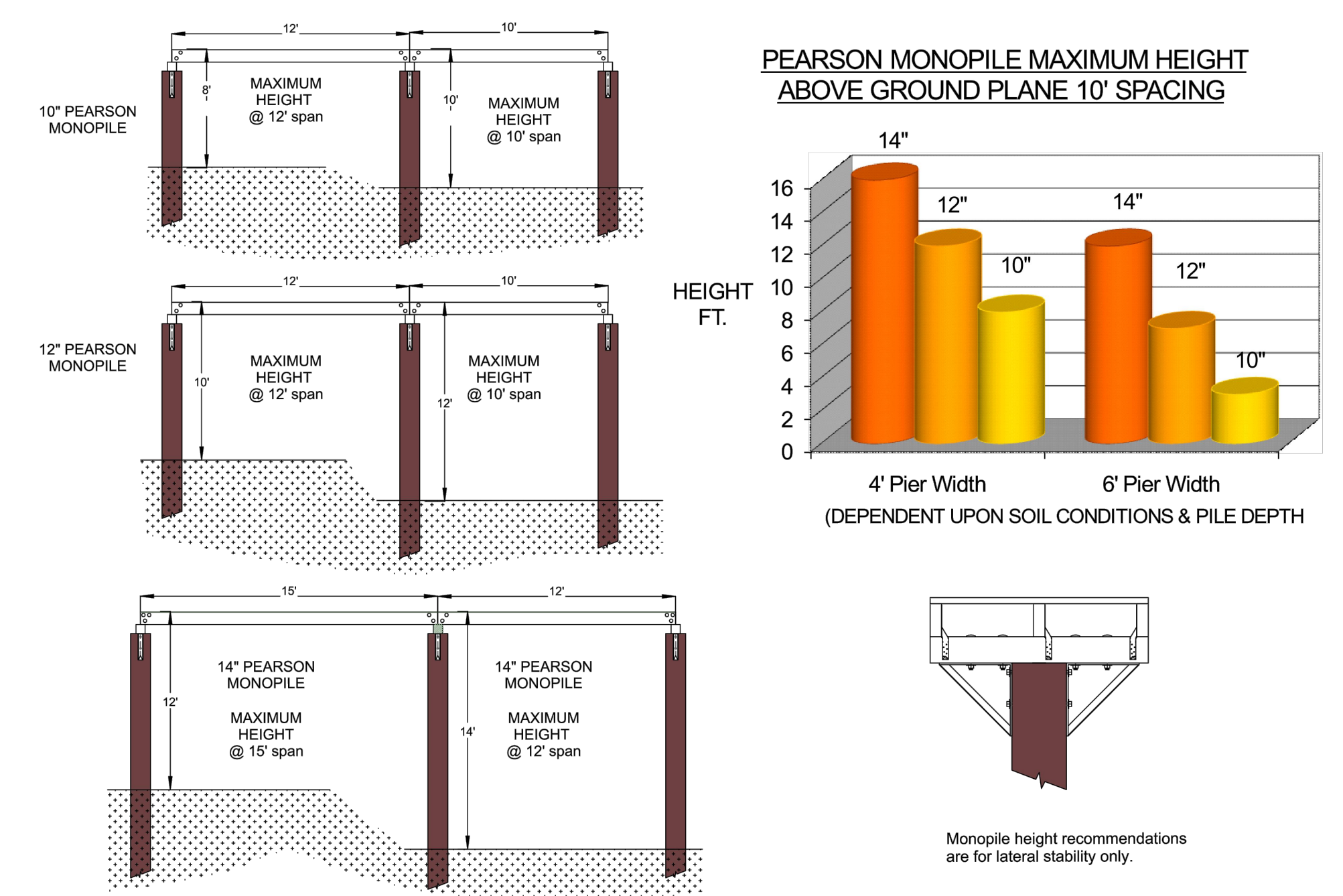
Bolt Hole Elongation - interior

The nominal working load of a 3/4" galvanized bolt is typically 4,400 lbs. and the yield of the composite pile wall (10" diameter) is 9,000 lbs. with a recommended capacity for bolt shear the same as the working load of the bolt.

Testing performed at the Kirk Laboratory, Civil Engineering Dept., University of Rhode Island © 2007 Pearson Pilings, LLC

Q1. What kind of pile drivers have you used on Pearson Piles?

A1. We have used drop, impact (hydraulic, pneumatic, diesel) and vibratory hammers with a sheet pile clamp to drive the composite piles with no problems and little or no damage to the cosmetics. What does seem to work best with vibratory hammers is a sheet pile clamp that grips one edge of the pile. We usually insert a 1/4 section of a pile cut-off to reduce cosmetic damage, but even without it we only damage 8" of the top. Normally this is cut off when capping the piles. A pile clamp works well, but the clamp pressure needs to be reduced and a wood plug inserted into the composite pile. The top 3-to-4 feet will then be trimmed off.

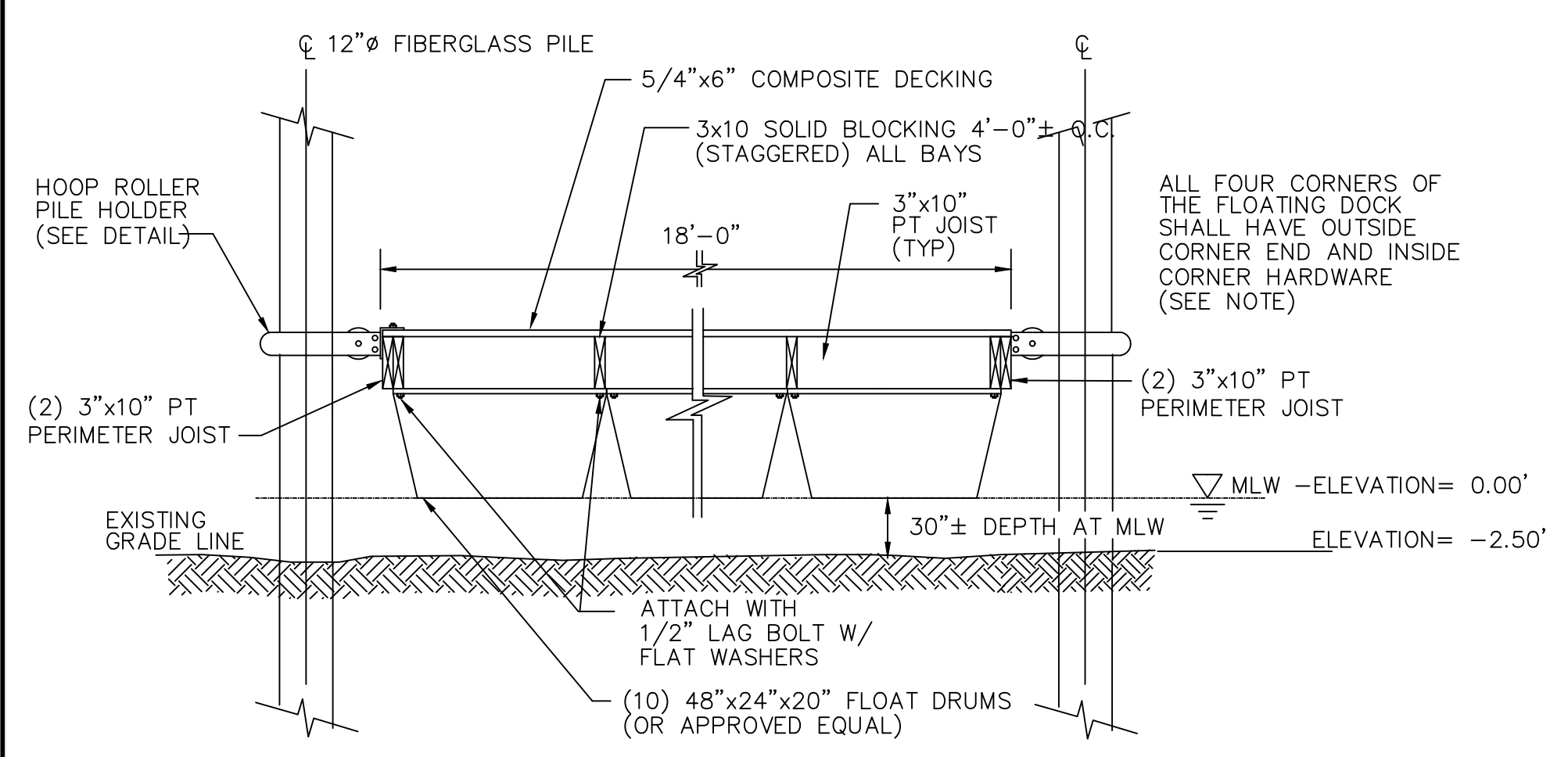


MONOPILE HEIGHT RECOMMENDATIONS

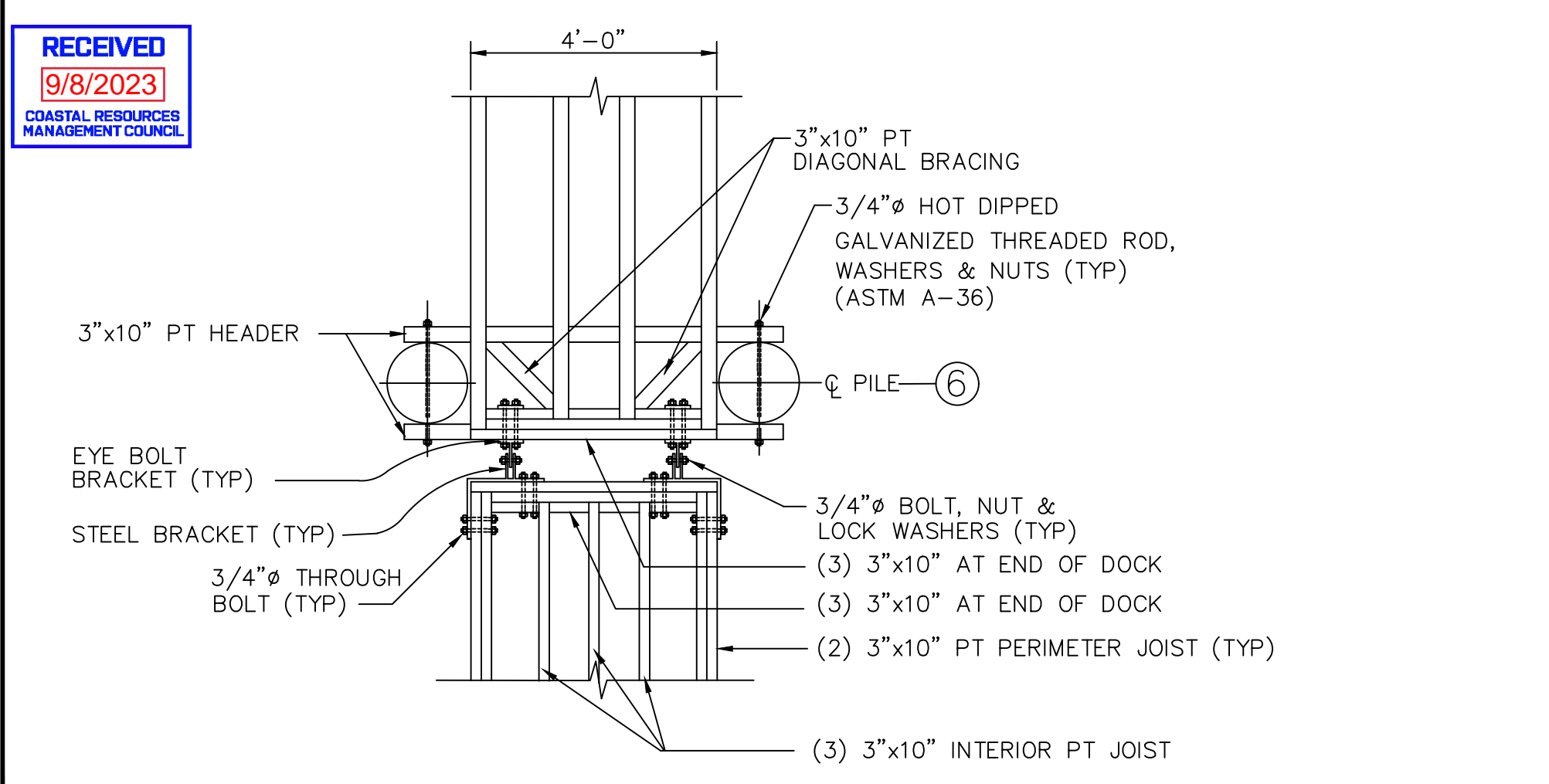
PEARSON Pilings LLC  
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Fall River, MA 02720  
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www.pearsonpilings.com

MONOPILE MATERIALS

PEARSON Pilings LLC  
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SECTION B-B  
SCALE: 1/2"=1'-0"



DETAIL C-PLAN VIEW  
SCALE: 1/2"=1'-0"

**Engineering Data - Pearson Composite Piles**



Materials Properties	Piling Diameter				
	8"	10"	12"	14"	16"
Reinforcement (grams/square meter)	2269	6072	7997	8329	10084
A quasi-isotropic three dimensional proprietary fabric utilizing e-glass grade filaments Exceptional damage tolerance with no crack propagation					
<b>Resin Matrix</b> An epoxy / vinyl ester, with high elongation, low styrene monomer, excellent hydrolytic stability and high heat deflection temperature, will not leach, inert, high chemical resistance, insoluble in any common hydrocarbons, mild acidic or alkaline solutions					
Mechanical Properties	Piling Diameter				
<b>*Minimum Values*</b>	8"	10"	12"	14"	16"
Axial Tensile Strength - psi	50,122	50,490	68,000	66,890	64,300
Axial Tensile Modulus - (MOE) - psi	4,547,780	3,530,000	4,030,000	4,100,000	3,960,000
Axial Flexural Strength - psi	58,400	79,650	89,400	91,450	89,600
Axial Compressive Strength - psi	43,320	67,000	76,800	77,460	74,800
Transverse Tensile Strength - psi	11,733	29,000	27,600	28,700	28,400
Transverse Tensile Modulus - psi	2,433,870	1,760,000	1,774,000	1,760,000	1,770,000
Interlaminar Shear Strength - psi	13,000	12,000	12,000	12,000	12,000
Effective Bending Stiffness - psi	1.190E+08	3.214E+08	9.333E+08	1.528E+09	2.507E+09
Young's Modulus	4,547,780	3,530,000	4,030,000	4,100,000	3,960,000
Poisson's Ratio	0.22	0.25	0.23	0.24	0.24
Allowable Bending Moment - kips-ft (FS = 2)	16	19	56	69	101
Allowable Axial Load - kips short column	100	210	280	515	800
Barcol Hardness	>50	>50	>50	>50	>50
Glass to Resin Ratio - by weight	-60.40	-60.40	-60.40	-60.40	-60.40
Aprox. Wall Thickness - inches	~.117	~0.250	~0.375	~0.375	~0.500
Aprox. Weight - lbs/ft	4	7	10	13	20
Thermal Expansion - in/in/°F	<.000014	<.000012	<.000006	<.000006	<.000006
Water Absorption - %	<.25	<.25	<.25	<.25	<.25

For more information contact:  
Pearson Pilings, LLC  
846 Airport Road  
Fall River, MA 02720  
508-675-0594  
www.pearsonpilings.com

\*Pearson Pilings does have the ability to customize laminates to meet the needs of your project should requirements exceed our standard piling specifications\*

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General Notes

Thomas J. Principe, III  
REGISTERED PROFESSIONAL ENGINEER

DETAILS PROVIDED BY:

PEARSON PILINGS, LLC  
846 AIRPORT ROAD  
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NEW DOCK PLANS  
for  
AP 25 LOT 45  
395 PARK AVENUE  
in  
PORTSMOUTH, RHODE ISLAND

Project	Sheet
Date: 04/28/2023	2 OF 3
Scale:	

CRMC DOCK NOTES: (Section 300.4 - Recreational Boating Facilities)

- The Executive Director or the Deputy Director may only grant a variance for the extension of a recreational or limited recreational boating facility out to 75 feet beyond MLW or up to a 50% increase beyond the fifty (50) foot standard (Section 300.4.E.3.1) provided engineering, biological, and other appropriate concerns are met.
- All residential and limited recreational dock designs shall be in accordance with Table 3 - Minimum Design Criteria, but in no case shall any structural member be designed to withstand less than 50 year storm frequency, including breaking wave conditions in accordance with ASCE 7 (current edition) and FEMA Manual 55. All design elements including the bathymetry shall be stamped by a Rhode Island registered Rhode Island Professional Engineer.
- Fixed structures which are for pedestrian access only shall be capable of supporting forty (40) pounds per square foot live load as well as their own dead weight; floating structures shall be capable of supporting a uniform twenty (20) pounds per square foot live load, or a concentrated load of four hundred (400) pounds. A written certification by the designer that the structure is designed to support the above design loads shall be included with the application.
- No creosote shall be applied to any portion of the structure.
- A residential or limited recreational boating facility shall be a maximum of four (4) feet wide, whether accessed by a fixed pier or float. The terminal float size shall not exceed one hundred fifty (150) square feet to be reviewed as a Category A application. A variance may be granted up to 200 square feet in excessive fetch areas, however this shall be reviewed as a Category B application at the full Council. In the absence of a terminal float, a residential boating facility may include a fixed terminal T or L section, no greater than four (4) by twenty (20) feet in size.
- All new or replacement floats shall utilize floatation that was specifically fabricated for marine use and warranted by its manufacturer for such use. Foam billets or foam bead shall not be utilized unless they are completely encapsulated within impact resistant plastic.
- Where possible, residential boating facilities shall avoid crossing coastal wetlands. In accordance with Section 300.17, those structures that propose to extend beyond the limit of emergent vegetative wetlands are considered residential boating facilities. Facilities shall be located along the shoreline so as to span the minimal amount of wetland possible. Facilities spanning wetlands shall be elevated a minimum of four (4) feet above the marsh substrate to the bottom of the stringers, or constructed at a 1:1 height to width ratio. Construction in a coastal wetland shall be accomplished by working out from completed sections. When pilings are placed within coastal wetlands, only the immediate area of piling penetration may be disturbed. Pilings should be spaced so as to minimize the amount of wetland disturbance. No construction equipment shall traverse the wetland while the facility is being built.
- Owners are required to maintain their facilities in good working condition. Facilities may not be abandoned. The owner shall remove from tidal waters and coastal features any structure or portions of structures which are destroyed in any natural or man-induced manner.
- Float ramps and other marine appurtenances or equipment shall not be stored on a coastal feature or any area designated as a CRMC buffer zone.
- The use of cribs for structural support shall be avoided. The use of cribs as support in tidal waters may be permitted given certain environmental design considerations. However, in these instances the size and square footage shall be minimized and the structure cannot pose a hazard to navigation. When cribs are permitted for structural support, they must be removed when the useful life of the structure has ceased (e.g. the structure is no longer used as a means of accessing tidal waters).
- Residential and limited recreational boating facilities shall not intrude into the area within twenty five (25) feet of an extension of abutting property lines unless (1) it is to be common structure for two or more adjoining owners, concurrently applying or (2) a letter or letters of no objection from the affected owner or owners are forwarded to the CRMC with the application. In the event that the applicant must seek a variance to this standard, the variance request must include a plan prepared by a RI registered Land Surveyor which depicts the relationship of the proposed facility to the effected property line(s) and their extensions.
- Residential and limited recreational boating facilities shall not extend beyond that point which is (1) 25% of the distance to the opposite shore (measured from mean low water), or (2) fifty (50) feet seaward of mean low water, whichever is the lesser.
- All residential and limited recreational docks, piers, and floats shall meet the setback policies and standards contained in municipal harbor management plans and/or harbor ordinances approved by the Council. However, in all cases, residential docks, piers, and floats shall be setback at least fifty (50) feet from approved mooring fields and three-times the U.S. Army Corps or Engineers authorized project depth from federal navigation projects (e.g., navigation channels and anchorage areas).
- The surface of the dock, pier and float shall be designed in a manner which provides safe traction and allows for the appropriate drainage of water.
- As part of a residential or limited recreational boating facility, the terminal float may be designed such that it facilitates the access of small vessels such as kayaks, dinghies, personal water craft, etc., onto the float, provided that all other programmatic requirements are met. Mechanical apparatus to accomplish this shall not exceed twenty four (24) inches in height from the top of the float.
- All residential and limited recreational docks shall have the centerline of the structure between its most seaward and most landward portion designated on the plans with State Plane Coordinates (NAD83). A WAAS enabled GPS system with an accuracy of +/- 3 meters shall be considered acceptable. The Executive Director shall have the discretion to require greater accuracy.
- Lateral Access shall be provided under, around or over as appropriate for the site conditions at all new residential docks.
- All residential and limited recreational docks shall be certified by the Design Engineer that it was constructed according to the approved plans within typical marine construction standards. The Executive Director shall have the discretion to require AS-BUILT survey plans of residential and limited recreational docks that includes property lines.

**E.3.1 Residential and Limited Recreational Docks with Excessive Fetch Standards**

- A location shall be considered to have excessive fetch if there is a 20° sector over four miles in any direction in which wind can blow over the water to generate waves.
- Boat lifts, suitably designed and installed, are encouraged for docks with excessive fetch.
- Residential and limited recreational docks with excessive fetch shall provide uplift calculations as part of the required calculation package.
- All structural elements, including the boat lift, shall be designed to withstand the 100 year storm frequency, including breaking wave conditions in accordance with ASCE 7 (current edition) and FEMA Manual 55.
- All residential and limited recreational docks with excessive fetch shall have an As-built plan on file with the CRMC within thirty (30) days of construction that certifies conformance with the approved plans.
- All residential and limited recreational docks with excessive fetch shall be inspected and certified by a Registered Professional Engineer licensed in Rhode Island that all elements of the dock and lift system meet the requirements of ASCE 7 (current edition) or FEMA Manual 55 every five (5) years.

**DESIGN CRITERIA PER TABLE 3**

- Min. Pile Tip diameter - 10"
- Min. Pile But diameter - 12"
- Residential Minimum Pile embedment - 10 feet
- Residential Deck load - 40 psf LL / 400 lb concentrated
- Min Float Freeboard - 12"
- \*including LL and DL
- Design Wind Loads - wind gust based on 50 year return and natural period of 60 seconds
- Wave Conditions (min) - All fixed and floating structure shall be designed for a 3'
- Min / Max Float freeboard - 8" / 30"
- Minimum Stringer/Joist - 3"x10"
- Minimum through bolt Hardware Diameter - 3/4" hot dipped galvanized
- Minimum Cross bracing - 3"x10"
- Minimum lag bolt diameter - 1/2"
- Minimum Water depth at the terminus of recreational boating facilities - 18" MLW
- Required Datum - MLW

Min Pile Cut Off	V zone elevation + float freeboard +1'
Steel or cast steel	490 pcf
Cast iron	450 pcf
Aluminum alloys	175 pcf
Timber (untreated)	40-50 pcf
Timber (treated)	45-60 pcf
Concrete, reinforced (normal weight)	145-155 pcf
Concrete, reinforced (lightweight)	90-120 pcf
Asphalt paving	150 pcf
Granite Block	165 pcf

**BREAKING WAVE LOAD ON VERTICAL PILE CALCULATION**

$$F = \frac{1}{2} C \gamma D H^2 = \frac{1}{2} (1.75)(64 \text{ lb/ft}^3)(1 \text{ ft})(13.26 \text{ ft})^2 = \frac{1}{2} (19,693) = 9,846 \text{ lb}$$

$$M = 9,846 \text{ lb} (17 \text{ ft}) = 167,388 \text{ ft-lb} / 5 \text{ piles} = 33,477 \text{ ft-lb}$$

- F = drag force acting at the stillwater elevation
- C = breaking wave coefficient (1.75 for round piles)
- γ = specific weight of salt water (64 lb/ft³)
- D = pile diameter
- H = breaking wave height at design stillwater depth (H = 0.78(17 ft) = 13.26 ft)
- M = moment applied by breaking wave load

**HYDRODYNAMIC LOAD ON VERTICAL PILE CALCULATION**

$$F = \frac{1}{2} C \rho V^2 A = \frac{1}{2} (1.2)(1.99 \text{ slug/ft}^3)(17 \text{ ft/s})(17 \text{ ft})^2 = \frac{1}{2} (11,732) = 5,866 \text{ lb}$$

$$M = 5,866 \text{ lb} (8.5 \text{ ft}) = 49,862 \text{ ft-lb} / 5 \text{ piles} = 9,972 \text{ ft-lb}$$

- F = hydrodynamic load acting at mid-depth
- C = drag coefficient (1.2 for round piles)
- ρ = density of salt water (1.99 slug/ft³)
- A = surface area of pile normal to flow
- V = velocity of water (V = ds/t = 17ft / 1sec = 17 ft/s)
- M = moment applied by hydrodynamic load

**DEBRIS IMPACT LOAD ON VERTICAL PILE CALCULATION**

$$F = W V C_D C_B C_{str} = (1,000 \text{ lb})(11.7 \text{ ft/s})(1.0)(1.0)(0.2) = 2,340 \text{ lb}$$

$$M = 2,340 \text{ lb} (17 \text{ ft}) = 39,780 \text{ ft-lb} / 5 \text{ piles} = 7,956 \text{ ft-lb}$$

- F = debris impact load in pounds
- W = weight of the object (recommended 1,000 lb weight)
- C<sub>D</sub> = depth coefficient (1.0 = for > 5 ft depth)
- C<sub>B</sub> = blockage coefficient (1.0 = for no upstream screening)
- C<sub>str</sub> = structure coefficient (0.2)
- V = velocity of water (V=1/2(g ds)^(1/2) = 1/2(23.4) = 11.7 ft/s)
- M = moment applied by debris impact load

**MAXIMUM BENDING MOMENT**

$$M_{max} = 33,477 + 9,972 + 7,956 = \boxed{51,405 \text{ ft-lb} = 51.4 \text{ kip-ft} < 56 \text{ kip O.K.}}$$

**VERTICAL UPLIFT FORCE ON PIER DECK**

$$F = \gamma h L W = (64 \text{ lb/ft}^3)(7.25 \text{ ft})(10 \text{ ft})(4 \text{ ft}) = 18,560 \text{ lb}$$

- F = vertical uplift force per pile from wave slam on pier deck
- γ = specific weight of salt water (64 lb/ft³)
- h = height of wave above pier deck (h = 17 ft - 9.75 ft = 7.25 ft)
- L = length of pier between piles (10 ft per design)
- W = width of pier deck (4 ft per design)

**BUOYANCY UPLIFT FORCE PER PILE**

$$F = \gamma (\text{vol.}) = (64 \text{ lb/ft}^3)(13.4 \text{ FT}^3) = 860 \text{ lb}$$

- F = upward buoyancy force per pile
- γ = specific weight of salt water (64 lb/ft³)
- vol. = volume of each pile (vol. = 17 ft x π (0.5')² = 13.4 ft³)

**MAXIMUM UPLIFT FORCE**

$$F_{max} = 18,560 + 860 = \boxed{19,420 \text{ lb} < 25,000 \text{ lb O.K.}}$$

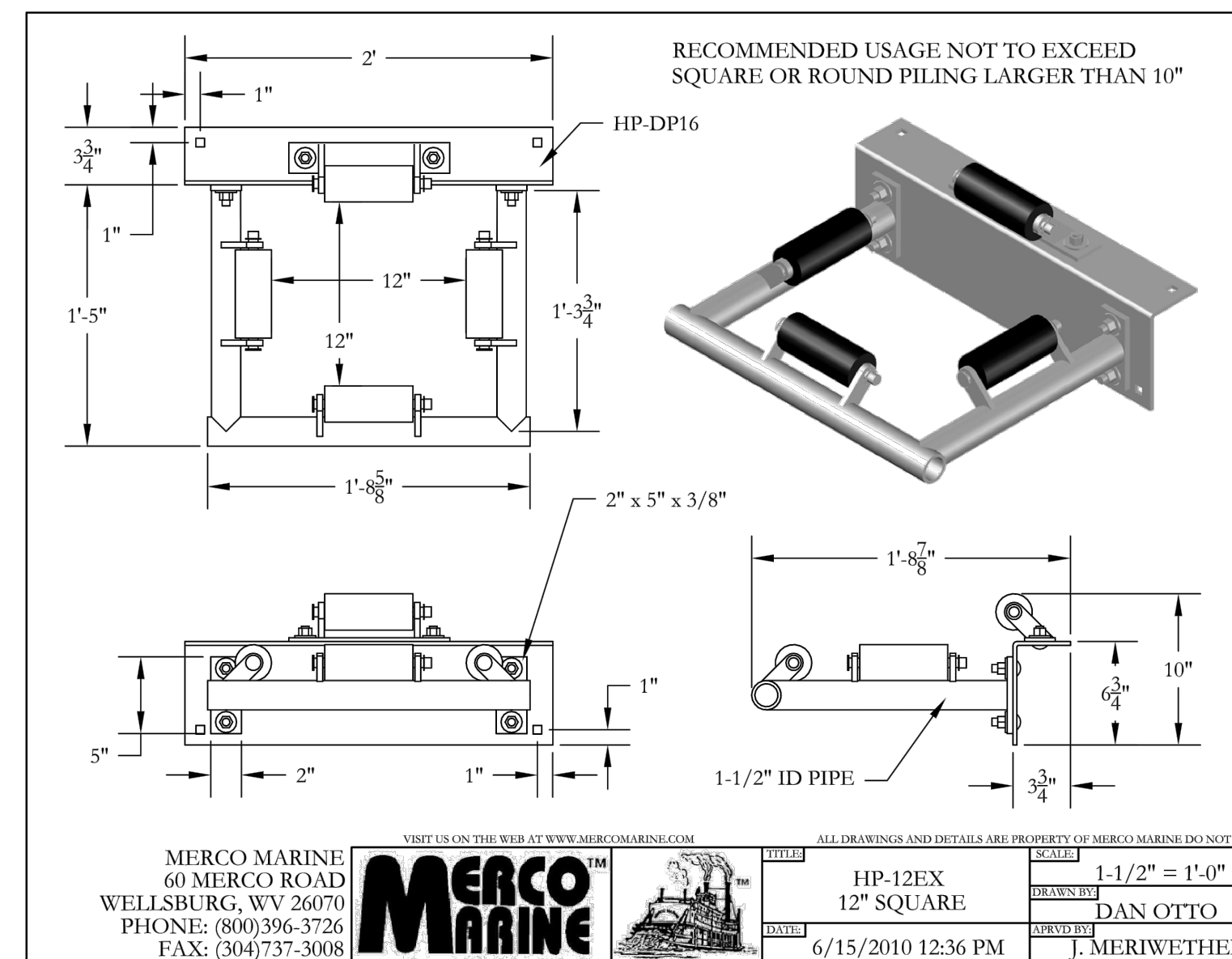
**NOTE: Pile driver to establish a minimum resistance of 25,000 lb per pile according to above uplift calculations. All work to be coordinated with engineer.**

**NOTES:**

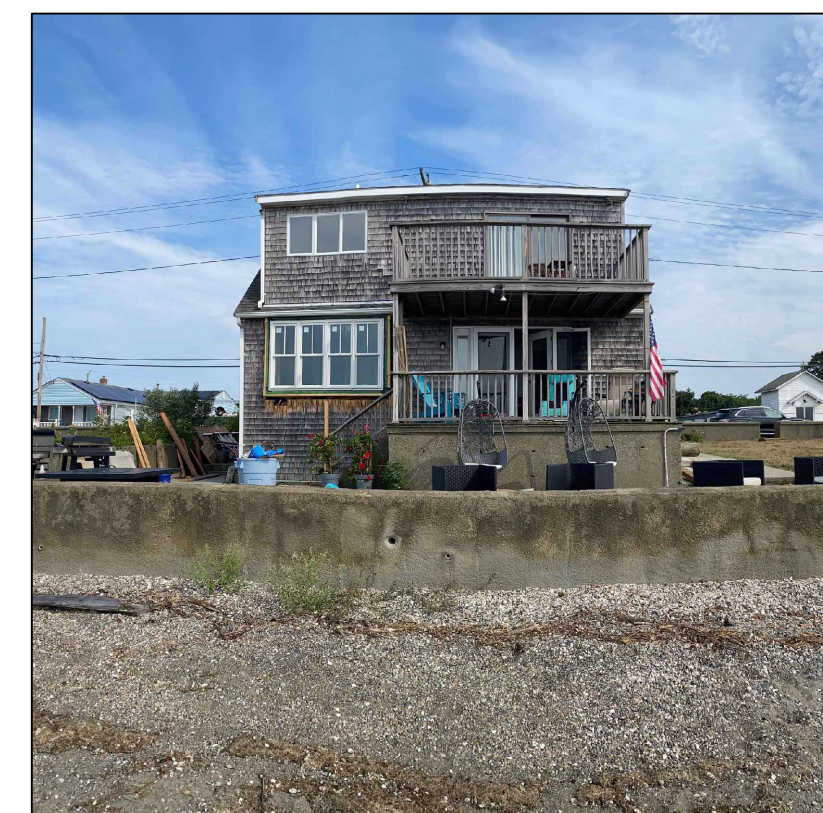
**HOOP PILE HOLDER**  
MOUNTING FRAME SHALL BE MADE FROM 1/4" MILD STEEL AND HOOP MADE FROM 1 1/2" SCHEDULE 40 STEEL PIPE. ALL MATERIALS ARE TO BE HOT-DIPPED GALVANIZED AFTER ALL WELDING AND FABRICATION IS COMPLETE. MOUNTING FRAMES SHALL USE 3/4" GALVANIZED CARRIAGE BOLTS FOR ATTACHMENT TO THE DOCK. HOOPS ARE TO BE ATTACHED TO THE MOUNTING BRACKET WITH 3/4" STAINLESS STEEL HEX HEAD BOLTS AND NYLOCK NUTS. THE ROLLER IS TO BE FABRICATED OF RUBBER. THE HOOP PILE HOLDER SHALL BE FOLLANSBEE SERIES PH-H OR EQUAL.

**FLOAT DRUMS**  
THE FLOAT DRUMS SHALL HAVE A HIGH DENSITY POLYSTHLENE (HDPE) SHELL FILLED WITH HIGH QUALITY EXPANDED POLYSTYRENE (EPS). EACH DRUM SHALL HAVE A 3" MOUNTING FLANGE MOLDED AROUND THE ENTIRE PERIMETER. A MINIMUM OF EIGHT (8) 1/2" LAG BOLTS WITH FLAT WASHERS SHALL BE USED TO ATTACH THE DRUMS TO THE DOCKS FRAMING ALL FLOAT DRUMS SHALL MEET STATE AND FEDERAL REQUIREMENTS FOR POSITIVE FLotation AND SHALL BE COAST GUARD APPROVED. THE FLOAT DRUMS SHALL BE FOLLANSBEE SERIES THREE FLOAT DRUM OR EQUAL.

**FLOATING DOCK HARDWARE**  
ALL FOUR OUTSIDE CORNERS SHALL HAVE OUTSIDE CORNER ENDS AND INSIDE CORNER HARDWARE. ALL HARDWARE SHALL BE HOT-DIPPED GALVANIZED 1/4" HIGH STRENGTH CARBON STEEL. ALL HARDWARE SHALL BE ATTACHED USING 3/4" GALVANIZED BOLTS WITH NYLON LOCK NUTS.



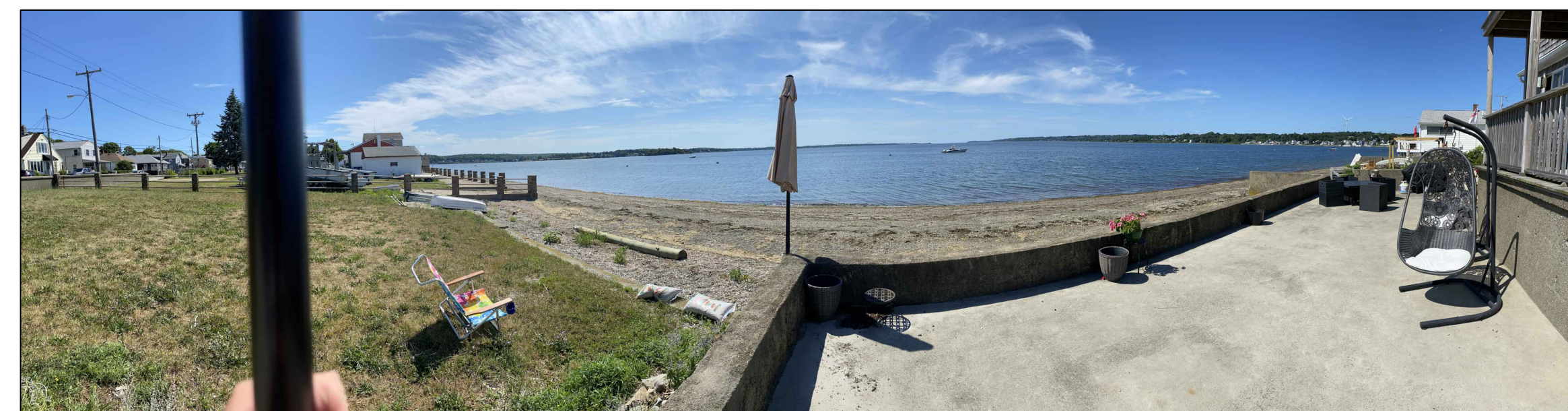
**SITE PHOTOS**



LOOKING NORTH



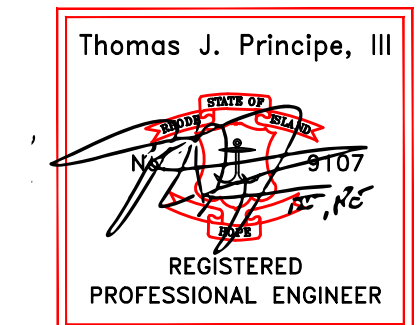
LOOKING WEST



LOOKING SOUTH



General Notes



DETAILS PROVIDED BY:

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395 PARK AVENUE  
in  
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Project	Sheet
Date 04/28/2023	3 OF 3
Scale	

NORTH

P A R K

(STATE HIGHWAY PLAT #508)

A V E N U E

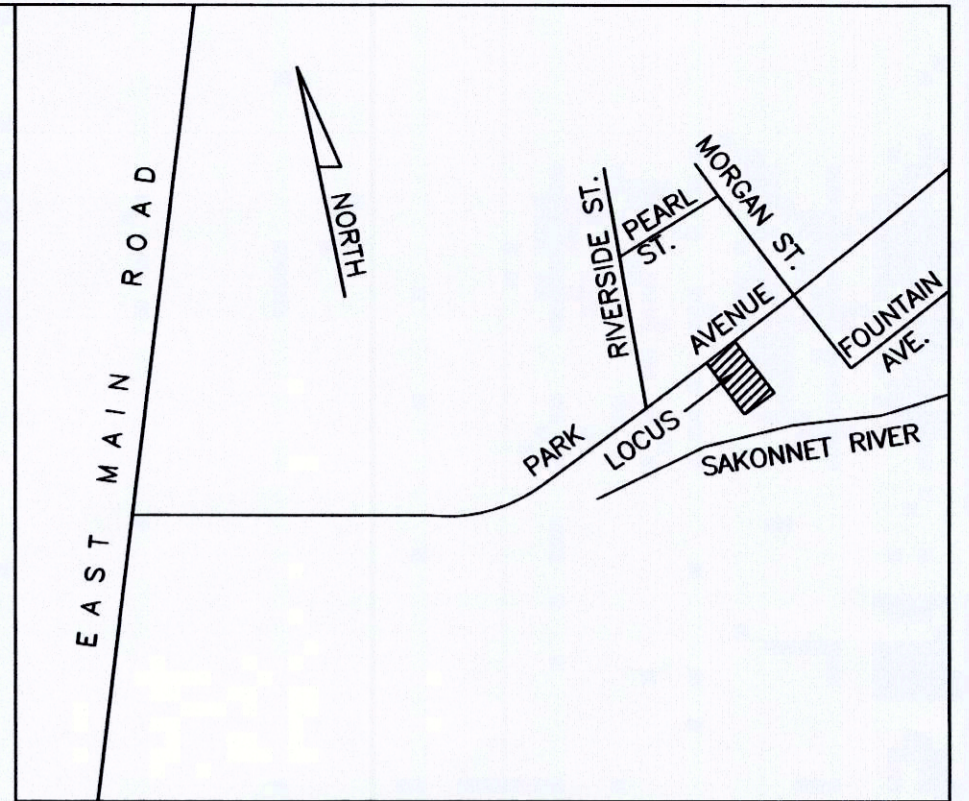
R.I.H.B(fnd s/of highway line)

HELD R.I.H.B AT sta:29+27.03 north side  
& R.I.H.B AT sta: 30+26.60 north side

52' PC STA: 42+30.54  
S.H.P. #508

### LEGEND

- R.I.H.B RHODE ISLAND HIGHWAY BOUND
- I.R. IRON ROD
- E.O.P. EDGE OF PAVEMENT
- D.H. DRILL HOLE
- MHW MEAN HIGH WATER
- UP UTILITY POLE
- P/L PROPERTY LINE



LOCATION MAP

EXISTING CURB LINE

UP#396

EXISTING SIDEWALK

EXISTING 18" WIDE CONCRETE RETAINING WALL

D.H.(set)

CH 34' 53"

L=20.08'

C-1

P/L

22.42'

90°

90° D.H.(set)

37.50'

18.50'

PLAT 25 LOT 46  
LAND N/F OF  
RINA LLC.

EXISTING HOUSE  
#395 PARK AVENUE

STOCKADE FENCE

PLAT 25 LOT 44  
LAND N/F OF  
TOWN OF PORTSMOUTH

PLAT 25  
LOT 43  
LAND N/F OF  
EST. OF  
CHARLES MAKIN

PLAT 25 LOT 45  
area: 3353 ± s.f.  
(L.E. BOOK 2078 PAGE 239)

EXISTING DECK

EXISTING CONCRETE RETAINING WALL

74.9'

83'

EXISTING CONCRETE RETAINING WALL

I.R.(set)

APPROX. 43.28'

MEAN HIGH WATER

I.R.(set)

SAKONNET RIVER

### PLAT REFERENCE

PLAN ENTITLED " PLAN OF OCEAN VIEW SITUATED IN PORTSMOUTH BELONGING TO C.S. GREENE , J.W. COUGHLIN & P.J. HURLEY " SURVEYED BY: E.M. CORBETT MAY 1900  
PLAN ENTITLED "STATE HIGHWAY PLAN #508"

### CURVE DATA

C-1  
DELTA: 0° 50' 13"  
RAD: 1374.42'  
TAN: 10.04'

### CERTIFICATION

THIS SURVEY HAS BEEN CONDUCTED AND THE PLAN HAS BEEN PREPARED PURSUANT TO 435-RICR-00-00-1.9 OF THE RULES AND REGULATIONS ADOPTED BY THE RHODE ISLAND STATE BOARD OF REGISTRATION FOR PROFESSIONAL LAND SURVEYORS ON NOVEMBER 25, 2015 AS FOLLOWS:  
TYPE OF BOUNDARY SURVEY: LIMITED CONTENT BOUNDARY SURVEY  
MEASUREMENT SPECIFICATION: CLASS 1 STANDARD

THE PURPOSE FOR THE CONDUCT OF THE SURVEY AND FOR THE PREPARATION OF THE PLAN IS AS FOLLOWS: TO SHOW THE EXISTING CONDITIONS OF THE PROPERTY WITHIN THE SURVEYED BOUNDARY LINES.

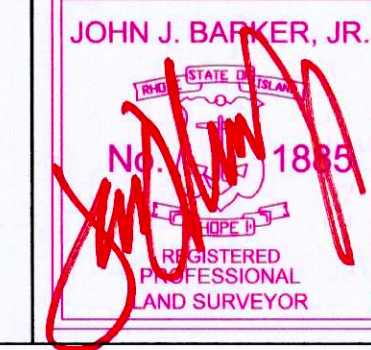
BY: *[Signature]*  
JOHN J. BARKER, JR. PLS # 1885  
C.O.A. # 15-A302

### EXISTING CONDITIONS

BARKER LAND SURVEYING, INC.  
168 HIGH ST BRISTOL R.I. 02809 (401) 254-0824

S I T E P L A N  
for  
Mark A. & Cheryl A. DeMello

395 PARK AVENUE PLAT 25 LOT 45 PORTSMOUTH R.I. 02871				
DWG NO.	SCALE	DATE	DWN BY	SHEET
211203-303	1"=10'	1/1/2022	JJB	1 OF 1



### REVISIONS

revised mean high water line 1/28/2022 jjb